

Application Note: Quick Guide on Automotive Load Dump Protection (ISO 16750-2) - Part 2

Understanding TVS Diode SPICE Simulation and Validation for ISO 16750-2 Load Dump Protection

1. INTRODUCTION

In **Part 1** of this application note, we examined automotive Load Dump events and the requirements defined by ISO 16750-2. We also reviewed the key TVS diode selection parameters required for automotive load dump protection, including *Reverse Working Maximum Voltage (V_{RWM})*, *Breakdown Voltage (V_{BR})*, *Clamping Voltage (V_C)*, *Peak Pulse Current (I_{PP})*, *Peak Pulse Power (P_{PP})*, and AEC-Q101 qualification.

While these parameters provide an initial basis for TVS selection, successful automotive surge protection requires more than simply meeting the minimum electrical requirements. A properly selected TVS diode must not only withstand the load dump transient defined by ISO 16750-2 but also operate with sufficient design margin to account for temperature effects, component tolerances, and long-term reliability requirements.

In this second part, we demonstrate how to validate a selected TVS diode for automotive load dump protection using analytical calculations, SPICE simulation, and experimental test data. SPICE simulation plays an important role during the design phase by allowing engineers to predict the behavior of the TVS diode under load dump conditions, verify critical parameters such as *clamping voltage* and *peak pulse power*, evaluate the suitability of the protection device before hardware testing.

Finally, the simulation results are correlated with actual load dump test data to demonstrate the effectiveness of the selected TVS solution under ISO 16750-2 test conditions. By combining calculation,

simulation, and validation testing, designers can achieve a more robust and reliable automotive load dump protection strategy.

2. SELECTING THE RIGHT TVS DIODE FOR ISO 16750-2 LOAD DUMP PROTECTION

Having established the key parameters required for automotive load dump protection in [Part 1](#), we can now proceed with the selection and validation of a suitable TVS diode. Based on the calculated load dump requirements for a 12V system, the **SM8S22CAHE3-TP** was selected from the TVS family evaluated according to a minimum V_{RWM} higher than 16V and a maximum V_C of 35V we can select the **SM8S22CAHE3** (TVS), on a DO-218AB package that enables high power dissipation in automotive applications for aggressive transients as the Load Dump. In this section, we demonstrate how SPICE simulation, analytical calculations, and component level laboratory testing can be used to validate the performance of the selected TVS diode under load dump conditions. We also show how to correlate the calculation, simulation, and test results to verify the suitability of the device and establish confidence in its long-term reliability for automotive applications.

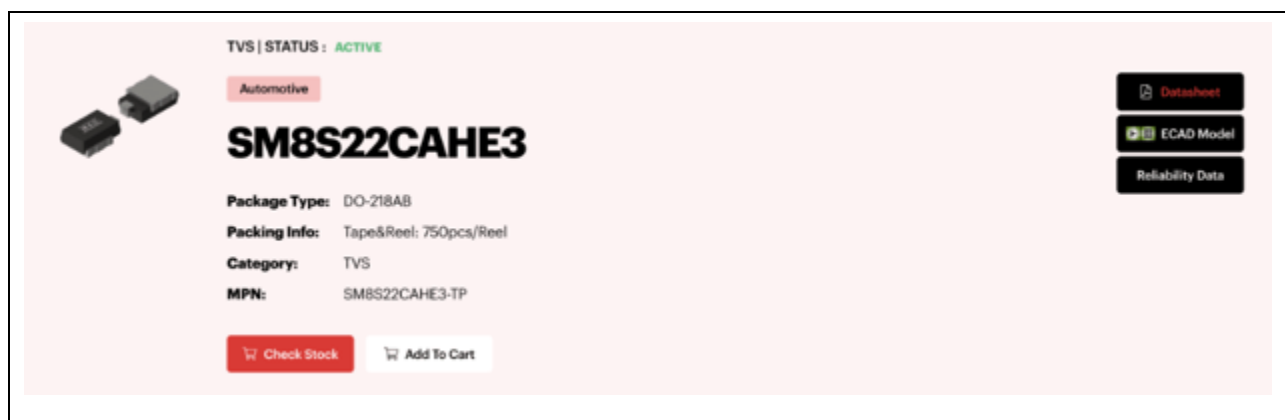


Figure 1: SM8S22CAHE3 product page

 SM8S10(C)AHE3 THRU SM8S85(C)AHE3									
Electrical Characteristics @ 25°C Unless Otherwise Specified									
Part Number	Working Peak Reverse Voltage V_{RWM}	Breakdown Voltage V_{BR} @ I_T			Maximum Reverse Leakage I_R @ V_{RWM}	Maximum I_R @ V_{RWM} $T_J=175^\circ\text{C}$	Maximum Reverse Surge Current I_{PP}	Maximum Clamping Voltage V_C @ I_{PP}	Marking Code
Bi	(V)	Min (V)	Max (V)	I_T (mA)	(μA)	(μA)	(A)	(V)	
SM8S10CAHE3	10	11.1	12.3	5.0	15	250	388	17.0	SM8S10CA
SM8S11CAHE3	11	12.2	13.5	5.0	10	150	363	18.2	SM8S11CA
SM8S12CAHE3	12	13.3	14.7	5.0	10	150	332	19.9	SM8S12CA
SM8S13CAHE3	13	14.4	15.9	5.0	10	150	307	21.5	SM8S13CA
SM8S14CAHE3	14	15.6	17.2	5.0	10	150	284	23.2	SM8S14CA
SM8S15CAHE3	15	16.7	18.5	5.0	10	150	270	24.4	SM8S15CA
SM8S16CAHE3	16	17.8	19.7	5.0	10	150	254	26.0	SM8S16CA
SM8S17CAHE3	17	18.9	20.9	5.0	10	150	239	27.6	SM8S17CA
SM8S18CAHE3	18	20.0	22.1	5.0	10	150	226	29.2	SM8S18CA
SM8S19CAHE3	19	21.1	23.3	5.0	10	150	213	30.8	SM8S19CA
SM8S20CAHE3	20	22.2	24.5	5.0	10	150	200	32.4	SM8S20CA
SM8S21CAHE3	21	23.3	25.7	5.0	10	150	187	34.0	SM8S21CA
SM8S22CAHE3	22	24.4	26.9	5.0	10	150	186	35.5	SM8S22CA
SM8S23CAHE3	23	25.5	28.1	5.0	10	150	173	37.1	SM8S23CA
SM8S24CAHE3	24	26.6	29.3	5.0	10	150	160	38.7	SM8S24CA
SM8S25CAHE3	25	27.7	30.5	5.0	10	150	147	40.3	SM8S25CA
SM8S26CAHE3	26	28.9	31.9	5.0	10	150	157	42.1	SM8S26CA
SM8S28CAHE3	28	31.1	34.4	5.0	10	150	145	45.4	SM8S28CA
SM8S30CAHE3	30	33.3	36.8	5.0	10	150	136	48.4	SM8S30CA
SM8S33CAHE3	33	36.7	40.6	5.0	10	150	124	53.3	SM8S33CA
SM8S36CAHE3	36	40.0	44.2	5.0	10	150	114	58.1	SM8S36CA
SM8S40CAHE3	40	44.4	49.1	5.0	10	150	102	64.5	SM8S40CA

Figure 2: Datasheet of SM8S22CAHE3

To further support the TVS selection process, this application note includes both SPICE simulation results and load dump qualification test report of the selected part number. While the calculations define the minimum electrical requirements and the simulation illustrates the expected transient response, the test report demonstrates the capability of the selected TVS diode under load dump conditions that are more demanding than those used in the design calculations.

This comparison shows that the simulated operating conditions are encompassed within the tested performance of the device, providing additional confidence that the selected TVS not only satisfies the calculated ISO 16750-2 requirements but also offers additional robustness for real-world automotive applications.

3. TVS SPICE SIMULATION – ISO 16750-2 TEST A

To obtain a more accurate representation of the performance of the selected TVS for this application, a brief SPICE simulation was performed, and the results were compared with the analytical calculations. It is important to note that this comparison focuses on evaluating the accuracy of the equations used during the TVS selection process, as the device had already been selected in the initial design step and the simulation is used solely to validate its expected behavior.

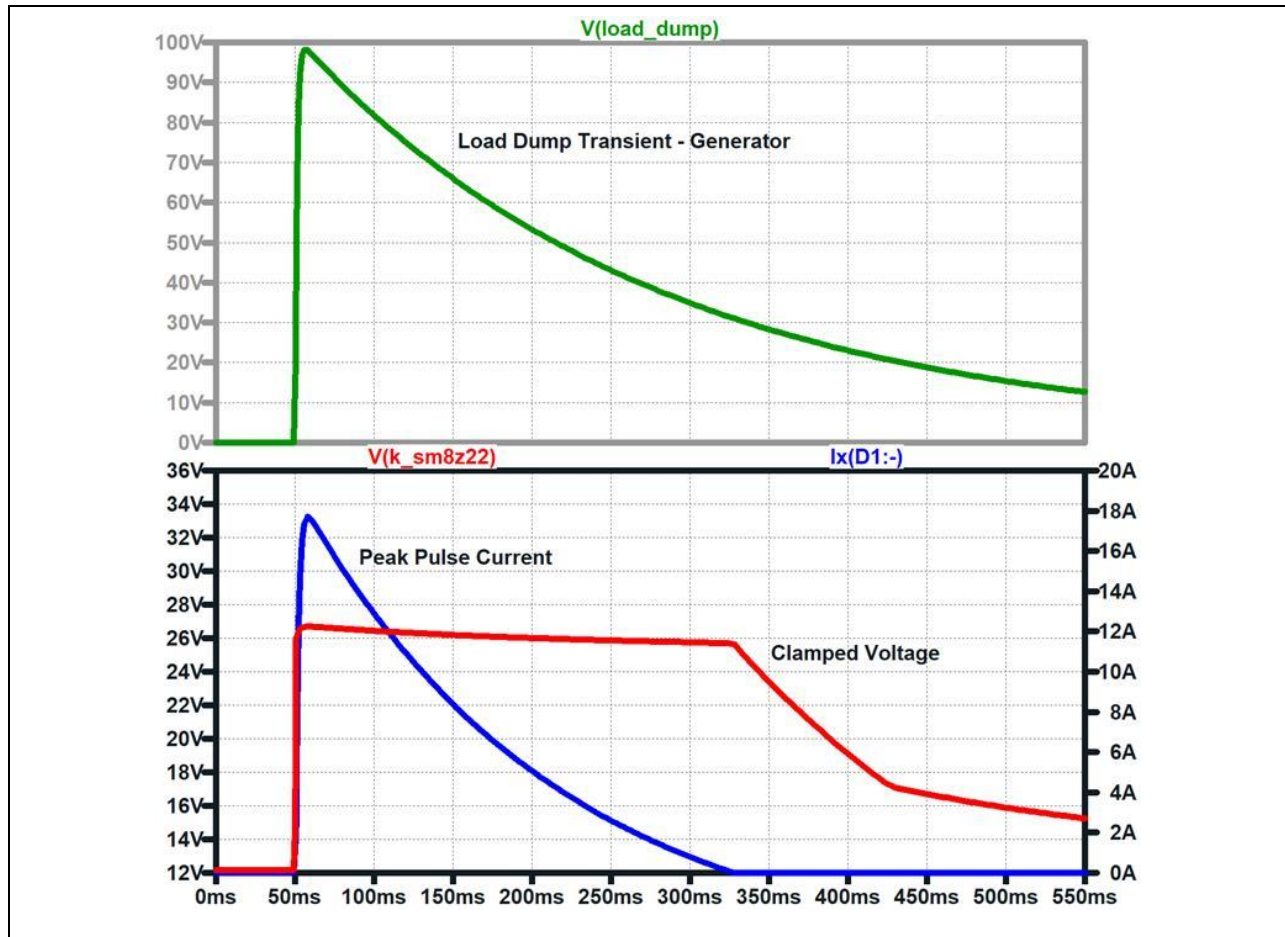


Figure 3: SPICE simulation results of TVS under Load Dump transient

Since the simulation uses fixed breakdown and clamping voltage values, the comparison focuses on the remaining parameters. In this case, the Load Dump generator provided by Analog Devices produces a *surge voltage* (V_P) of **98.512V**, compared to the **101V** defined by ISO specifications and used in the calculations. The simulated *clamping voltage* (V_C) is **26.697V**, while the maximum value established for

calculation was **35V**. Similarly, the simulated *peak pulse current* (I_{PP}) reaches **17.638A**, compared to the calculated value of **16.5A**.

For the *peak pulse power* (P_{PP}), the simulation yields **470.88W**, whereas the analytical calculation predicts **577.5W**. Additionally, the time at which the *peak pulse current* (I_{PP}) decays to 50% occurs at **84ms** in the simulation, while the calculated value was **88ms**. Refer to Table 1 for side-to-side comparison of these values.

Although slight deviations are observed between the SPICE simulation and analytical results, these differences are expected and remain within an acceptable range for engineering evaluation. The analytical calculations were intentionally based on conservative design parameters and worst-case conditions defined by ISO 16750-2 to support robust TVS diode selection for automotive Load Dump protection. In contrast, the SPICE simulation evaluates the behavior of the selected TVS diode under a specific load dump transient, providing a more realistic representation of its response.

It is also important to note that the analytical calculations utilize the upper limits specified by ISO 16750-2 for *surge voltage* (V_P), *pulse duration* (t_d), and *internal resistance* (R_i). In the SPICE simulation, several parameters differ from these worst-case assumptions, most notably the *surge voltage* (V_P), *peak pulse current* (I_{PP}), and *clamping voltage* (V_C). As a result, some variation between the calculated and simulated values is expected. Despite these differences, both methods demonstrate similar trends and confirm the suitability of the selected TVS diode for Load Dump protection.

In Table 1, both methods are set to use the same conditions. Once this is done, they are very similar to each other with a slight difference in *pulse duration* (t_P) and *peak pulse power* (P_{PP}) which concludes as acceptable results between calculation and simulation on SPICE.

Parameter	Symbol	SPICE Measurements	Design with Simulation Values	Calculated Theoretical Values	Unit
Surge Voltage	V_P	98.512	98.512	101	V
Clamping voltage	V_C	26.697	26.697	35	V
Internal Impedance	R_i	4	4	4	Ω
Breakdown voltage	V_{BR}	25.6	25.6	26.9	V
Transient duration	Load Dump	400	400	400	ms
Peak Pulse Current	I_{PP}	17.638	17.954	16.5	A
Peak Pulse Power	P_{PP}	470.88	479.31	577.5	W
Calculated Values With Measurements			Calculated Values		
Time constant Tau	τ	173.718	173.718	169	ms
Pulse duration	t_p	84	82	88	ms
50% Power Margin	-	706.3	719.0	866.3	W

Table 1: Comparison of Analytical Calculation, SPICE Simulation, and Measured Results for ISO 16750-2 Load Dump Validation

4. ISO 16750-2 LOAD DUMP TEST RESULTS AND TVS VALIDATION

While calculating a TVS diode for protection of overvoltage on our circuits is a good approach, we want to ensure the reliability of the device on the real-life application, therefore the selected part number was experimentally validated by our team to confirm, beyond simulation and analytical calculations, that this TVS family is suitable for surge events such as the Load Dump. The following figures show the test conditions and resulting waveforms for the **SM8S22CAHE3** TVS device under Test A conditions.

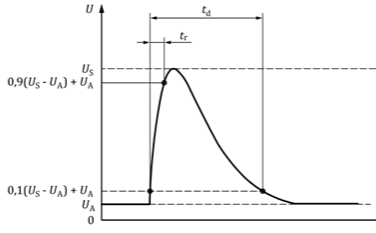
SM8S22CAHE3		Package type: DO-218AB	
General Specification: ISO 16750-2		Test site: Yangzhou, China	
Test pulse		Test Condition	
Pulse 5a		UA: 12 V US: 79~101 V Ri: 0.5~4Ω td: 400 ms tr: 10 ms COUNT: 5 pulses 固定US,TD, RI递增0.5 往上摸底, 如Ri=4Ω不过 , 则降低US摸底测试	

Figure 4: Test conditions for SM8S22CAHE3 TVS under Load Dump pulse

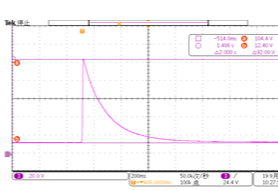
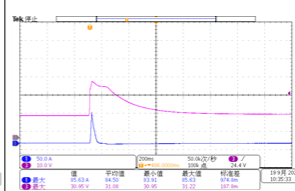
Product Series: TVS								
Ambient Temperature: 24℃ Humidity: 40%								
Test level	Sample size	Result Fail/Total	Result	Remark	测试前空波	测试波形	VC/V	IPP/A
III	5pcs	101V-0.5Ω0/5	101V-0.5ΩACC				30.95	85.63

Figure 5: Test results for SM8S22CAHE3 TVS under Load Dump pulse

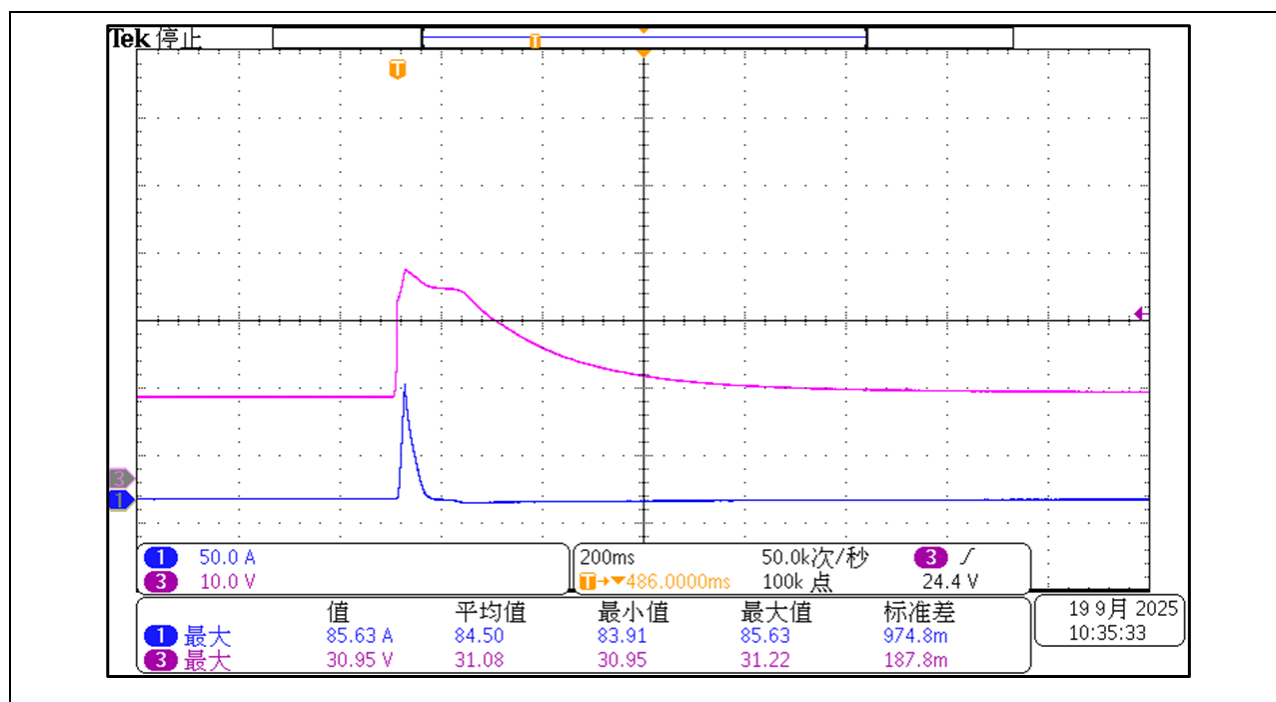


Figure 6: Current and Voltage waveform of TVS during Load Dump transient

5. CORRELATION BETWEEN ANALYTICAL CALCULATION, SPICE SIMULATION, AND LOAD DUMP TEST RESULTS

The analytical calculations presented in **Part 1** establish the electrical requirements required for selecting a suitable TVS diode under ISO 16750-2 load dump conditions. By adopting conservative assumptions and worst-case design parameters, the calculations provide a robust foundation for initial device selection.

The SPICE simulation further validates the analytical methodology by reproducing the transient behavior of the selected TVS diode under the defined load dump conditions. Although small deviations exist due to differences in surge voltage, clamping voltage, and pulse characteristics, the simulation closely follows the analytical predictions and confirms the suitability of the selected device.

Finally, the ISO 16750-2 load dump qualification test report provides the highest level of validation. Unlike the analytical calculations, which are based on design requirements, the qualification test subjects the

TVS diode to repeated load dump pulses under more demanding conditions. The successful completion of these tests demonstrates that the selected **SM8S22CAHE3** not only satisfies the calculated requirements but also provides additional design margin for real-world automotive applications.

Together, the analytical calculations, SPICE simulation, and qualification test results establish a complete verification methodology that increases confidence in the TVS selection process while improving the robustness and long-term reliability of automotive surge protection designs.

6. CONCLUSION

This two-part application note presented a practical methodology for selecting and validating a TVS diode for automotive load dump protection in accordance with ISO 16750-2.

Part 1 introduced the load dump phenomenon, explained the key TVS diode selection parameters, and demonstrated a step-by-step calculation method for determining the required *Reverse Working Maximum Voltage* (V_{RWM}), *Breakdown Voltage* (V_{BR}), *Clamping Voltage* (V_C), *Peak Pulse Current* (I_{PP}), and *Peak Pulse Power* (P_{PP}). Part 2 extended this methodology by validating the selected TVS diode through SPICE simulation and ISO 16750-2 load dump qualification testing. The close correlation between analytical calculations, simulation, and qualification test results confirms the effectiveness of the design approach while demonstrating that the selected TVS diode provides additional design margin beyond the calculated requirements.

By combining analytical calculations, simulation, and qualification testing, engineers can develop more robust automotive surge protection solutions, reduce design risk, and accelerate product development for ECUs, battery management systems (BMS), DC-DC converters, power distribution modules, infotainment systems, and other vehicle electronic systems exposed to load dump transients.

To support a wide range of automotive surge protection requirements, MCC offers a comprehensive portfolio of AEC-Q101 qualified TVS diodes specifically designed for ISO 16750-2 load dump protection in the robust DO-218AB package. The portfolio includes the **SM8S Series (6.6 kW)** and **SM8Z Series (8.0 kW)**, providing multiple power ratings to meet different automotive design requirements. Whether designing compact electronic control units or high-power automotive systems, engineers can select the most

appropriate TVS solution while maintaining compliance with demanding automotive surge protection standards.

Explore the complete [MCC Automotive Load Dump TVS portfolio](#) and datasheets to find the right protection solution for your next automotive power design. To help engineers further understand transient protection, automotive reliability, and TVS diode selection, MCC has developed a comprehensive collection of technical resources covering TVS fundamentals, application design, and real-world implementation. Continue Exploring MCC's TVS Protection Knowledge Center:

- [Understanding TVS Diodes: A Comprehensive Guide](#)
- [Three Fascinating Facts About TVS Diodes](#)
- [Safeguarding Sensitive Electronics: The Importance of TVS Diodes](#)
- [Application Note: Enhancing Data Center Reliability with TVS Diodes in Hot-Swap Controllers](#)
- [Made for Harsh Environments: MCC's Automotive-Grade TVS Series](#)

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